

# **Secondment Report Form**

Secondee	
Host Organization	Id: TNO
	Name: Netherlands Organization for Applied Scientific Research
Research Topic(s)	Cross-polarization reduction techniques in phased arrays
	Antenna CAD tools evaluation

#### ACTIVITIES DURING THE SECONDMENT

The aim of this section is to describe the main activity developed during my stay at TNO, Netherlands Organization for Applied Scientific Research.

The activity can be divided in two sections:

#### Section 1

*Scope*: study and evaluate techniques to reduce the field cross-polarization components for an antenna configuration consisting of two orthogonal dipoles set along y-axis and x-axis (see Fig 1).

### Section 2

*Scope*: evaluate the computation time performances of the ADF CAD tool when applied to the analysis of large array antennas (consisting of connected array of dipoles larger than 16x16 elements with an inter element distance of lambda/2).

The scope of the present document is limited to the CARE project.

### Section 1.

Figure 1 shows the antenna configuration studied in order to investigate cross-polarization reduction techniques. Two orthogonal dipoles are centred in the origin and assumed to be half-wave long at the frequency of analysis.

The co-polar and cross-polar components are defined as the component of the electric field vector normal and parallel to a desired vector, respectively.

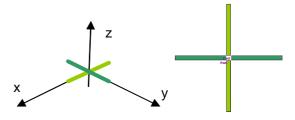


Figure 1: Crossed Dipoles

There are different definitions of Co and Cross, depending on the choice of the desired vector; for phased arrays and direct radiating antennas, the **Ludwig's third definition** is typically used, which leads to the following expressions of the co-polar and cross-polar fields radiated by the dipoles:

$$Cross_{y} = \cos\phi E_{y\theta} - \sin\phi E_{y\phi} = j\eta \frac{kI_{0}le^{-jkr}}{4\pi r} (\cos\theta \sin\phi \cos\phi - \sin\phi \cos\phi)$$

$$Co_{y} = \sin\phi E_{y\theta} + \cos\phi E_{y\phi} = j\eta \frac{kI_{0}le^{-jkr}}{4\pi r} (\cos\theta \sin\phi \sin\phi + \cos\phi \cos\phi)$$

$$Cross_{x} = \sin\phi E_{x\theta} + \cos\phi E_{x\phi} = j\eta \frac{kI_{0}le^{-jkr}}{4\pi r} (\cos\theta \cos\phi \sin\phi - \cos\phi \sin\phi)$$

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$$Co_x = \cos\phi E_{x\theta} - \sin\phi E_{x\phi} = j\eta \frac{kI_0 le^{-jkr}}{4\pi r} (\cos\theta\cos\phi\cos\phi + \sin\phi\sin\phi)$$

In order to reduce the cross-pol associated with the dipole along x (x-dipole), a weight  $\mathbf{q}(\theta, \phi)$  can be multiplied to the amplitude of the dipole along y (y-dipole), as follow:

$$Co_y = q(\theta, \phi)_{j\eta} \frac{kI_0 le^{-jkr}}{4\pi r} (\cos\theta\sin\phi\sin\phi + \cos\phi\cos\phi)$$

$$Cross_y = q(\theta, \phi)_{j\eta} \frac{kI_0 l e^{-jkr}}{4\pi r} (\cos\theta \sin\phi \cos\phi - \sin\phi \cos\phi)$$

This weight is a function of the observation angles  $\theta$  and  $\phi$ . The basic idea to reduce the cross-polarization of the x-dipole is to choose the weight  $q(\theta,\phi)$  so that the following equation is satisfied:

$$q(\theta, \phi)Co_y = -Cross_x$$

With this choice of  $q(\theta, \phi)$  the co-pol of the y-dipole cancels out with the x-pol of the x-dipole. Figure 2 shows the co-polar and cross-polar components of the x-dipole as a function of  $\theta$  and for  $\phi$ =45°. Analytical expressions (implemented via Matlab) are compared with simulations from Ansoft Designer.

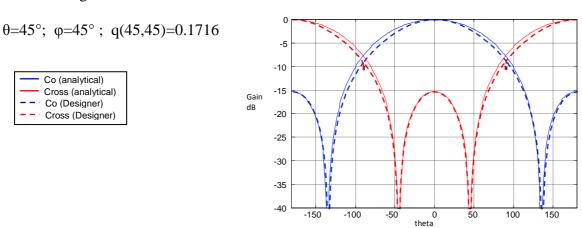


Figure 2: Cross-pol and co-polar - q(45,45)=0.1716

The value  $q(\theta, \phi)$  is calculated for  $\theta$ =45° and  $\phi$ =45°, and thus the **cross component shows a null** for the angle (45°,45°). Figure 3 refers to  $q(70^{\circ},45^{\circ})$ , so the cross-pol of the x-dipole vanishes at  $\theta$ =70° and  $\phi$ =45°.

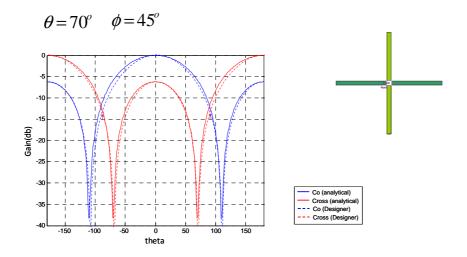


Figure 3: Cross-pol and co-polar - q(70,45)=0.1716

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Two orthogonal dipoles with shifted phase centres can also be considered (Figure 4).

In this case, in order to eliminate the cross-polar component of the x-dipole, the weight  $q(\theta, \varphi)$  has to be multiplied for a phase term accounting for the distance between the dipole centers:

$$e^{j\frac{2\pi d_x}{\lambda \frac{1}{2}}\sin\theta\cos\phi}e^{j\frac{2\pi d_y}{\lambda \frac{1}{2}}\sin\theta\sin\phi}$$

Figure 5 shows co and cross components for  $\theta$ =45° and  $\varphi$ =45°. Also in this case the cross polar component has a null at  $(45^{\circ},45^{\circ})$ .

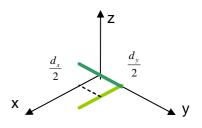
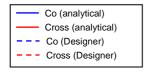


Figure 4: Shifted dipoles

 $\theta = 45^{\circ}$ ;  $\varphi = 45^{\circ}$ ;



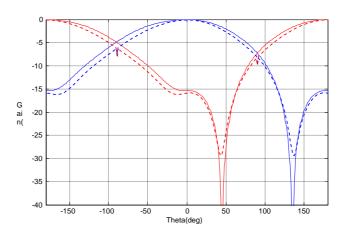


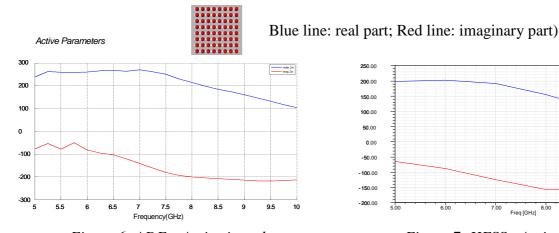
Figure 5: Cross-pol and co-polar - q(45,45)=0.1716

## **Section 2**

I studied and designed a connected array in free space, constituted by 256 dipoles with an inter element distance of lambda/2.

In order of reduce the calculation time with respect to other commercial EM solvers, the Antennas Designer Framework (ADF) can be used.

ADF is an antenna workbench, developed by IDS Company, where the user finds a suite of different modelling tools (multi-methods environment), both general purpose and specialised, able to co-operate in the formation of complex modelling procedures (combined methods procedures).



*Figure 6: ADF – Active impedance* 

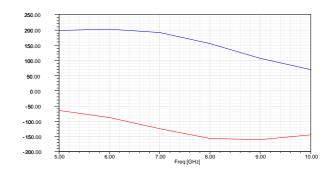


Figure 7: HFSS - Active impedance

**Public** Page 3 of 5 Comparing the active impedance of a central element of the array obtained via ADF and Ansoft HFSS (Figures 6 and 7), the same dynamic can be observed.

In the ADF case, the simulation time is lower: CPU Time: 37 min for frequency.

These results can be deepened.

MAIN RESULTS OF THE STAY			
Number of Publications:1	Other(s): (1)expected at EuCAP2011 (TBC)_		
Number of Documents/ Reports:	(2)		
Number of Case Studies & Demonstrators:	(3)		
* Attach all relevant documentation that specifies your results			
FORECAST ACTIVITIES			
In order to improve CARE's secondment program, pleat the end to expand your answers, if needed. Our aim secondees in future.	Disagree ← ➤ Agree		
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Other questions/comments to be potentially considered:	
The secondment experience resulted very positive from the technical an	d the coordination point of
view.	
In particular, the TNO matched the expectation in being ax extraordinar	y technical place where to
study the state-of-the-art techniques in antenna array design.	
Finally, I would like to express my thanks to the entire TNO staff that s	upported my secondment.
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SIGNATURES	
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Candidate Claudia Casali	Date:
	(year/month/day)
Signature	

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